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Multiscale Modeling of Recrystallization

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depends both on the value of the fractal radius to the lower cut-off of fractality. The
primarily determined by the stability of
and the ratio of distance between
that fragmentation will take place when comparable with the size of cluster) and
many particle will exceed a certain value, instability of the fractal aggregate.

...dependency on the geometry of the initial particle gyration radius, \( R_g \), and the value of the
he evolution were determined:
yed on the small lengthscales; however, on
of fractality, \( R_\alpha \) and gyration radius, \( R_g \),
of the initial particle (for large \( R/R_g \)) and
1 of a fractal particle without
rent from the homogeneous case,
the apparent value of the scaling exponent
on \( \alpha \) presumably reaches the value of 1/3.

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MULTISCALE MODELING OF RECRYSTALLIZATION

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ABSTRACT

We propose a multi length scale approach to modeling recrystallization which links a dislocation
model, a cell growth model and a macroscopic model. Although this methodology and linking
framework will be applied to recrystallization, it is also applicable to other types of phase
transformations in bulk and layered materials. Critical processes such as the dislocation structure
evolution, nucleation, the evolution of crystal orientations into a preferred texture, and grain size
evolution all operate at different length scales. In this paper we focus on incorporating experimental
measurements of dislocation substructures, misorientation measurements of dislocation
boundaries, and dislocation simulations into a mesoscopic model of cell growth. In particular, we
show how feeding information from the dislocation model into the cell growth model can create
realistic initial microstructures.

INTRODUCTION

The role of recrystallization models is to predict the influence of external variables such as strain,
strain rate, and temperature on microstructure and texture. Macroscopic models characterize the
microstructure in terms of state variables, such as dislocation content, cell size and texture [1].
These are related to the external variables via constitutive equations of recrystallization and
recovery derived either analytically or empirically by fitting to experiment. Macroscopic models have
achieved considerable success when applied systematically to specific systems of interest,
such as multi-pass rolling of steels [2,3]. However they do not include any details about the
microstructure of the alloy, except in terms of average properties. It is becoming increasing clear
that heterogeneities present in the microstructure greatly influence the nucleation process [1,4].

Deformation microstructures consist of cellular patterns of dislocation boundaries. In so much
that this is similar to a grain structure, it might seem that the Monte Carlo Potts model would be
well suited to simulate evolution of such a structure. The Potts model is extremely successful in
modeling annealing processes such as grain growth [5], and secondary recrystallization [6]. It has
been applied to primary recrystallization by a number of workers, but in all cases nucleation has
been imposed on the simulation either by directly inputting nuclei [7] or by imposing nucleation
criteria [8]. In both cases the model is employed as a macroscopic model to investigate the effect
of heterogeneous nucleation on the final microstructure and texture. These studies do not reveal
information about the nucleation mechanism of recrystallization.

The central question is how do high angle recrystallization nuclei emerge from an evolving
structure of dislocation boundaries? There is currently a great deal of experimental work
characterizing dislocation substructures. Since it is not feasible to map out the deformation
structure of a material, structural laws need to be developed through statistical sampling of small
volumes using the TEM. This approach has been pioneered by Hughes et al.[9] who have
proposed a scaling law for dislocation boundaries in medium to high stacking fault fcc
metals. Such work is important because these laws can allow models of cell growth to incorporate
realistic starting microstructures. Experimental work to elucidate the kinetic law for the motion of
dislocation boundaries is also a vital piece of the jigsaw. Many workers have assumed that
dislocation boundaries will migrate under curvature driven growth. It is not clear that this is valid;
in particular one would expect dislocation climb and glide to greatly influence boundary migration.

We model recrystallization using a multiscale approach. A dislocation model is employed to examine the dynamics of dislocation cell structures and in particular to develop a kinetic law for dislocation boundary motion. This is fed into a mesoscopic simulation in which we model boundaries instead of dislocations, allowing us to model 3D microstructures and simulate a large number of cells. The initial boundary misorientation distribution (BMD) is compared to the experimental BMDs measured by Hughes et al [9]. Parameters such as nucleation rates and nuclei orientation are fed from the mesoscopic model into a macroscopic model of recrystallization.

In this short paper we describe briefly the dislocation model and the cell growth model, and show how feeding information between them enables us to develop realistic starting microstructures which compare well with experiment.

DISLOCATION MODEL

A 2D Monte Carlo dislocation model was used to create experimentally realistic dislocation cell structures. The simulation volume was discretized into a triangular lattice with periodic boundary conditions and Burger vectors along each principle direction. The initial configuration consisted of N randomly placed edge dislocations. The energy of the system was defined in terms of the sum of the potential between pairs of dislocations (i, j) in the system. Using the stress tensor of a periodic array of dislocation (j), the force on another dislocation (i) can be calculated using the Peach-Kohler equation. The interaction potential between the dislocations is then given by [10]:

$$\Phi_q = \int (\sigma_{xj} b_{1x} + \sigma_{yj} b_{1y}) dy$$

where $\sigma_{xj}$ and $\sigma_{yj}$ are components of the stress tensor of dislocation (j) and $b_{1x}$ and $b_{1y}$ are components of the burgers vector of dislocation (i) in the x and y directions. The energy, $E$, of the system is the sum of the interaction potentials. The system is relaxed using a Monte Carlo method. A dislocation is chosen at random and the change in energy, $\Delta E$, associated with a proposed move of unit distance along its slip direction is calculated. This move is accepted if $\Delta E < 0$. At present the simulation does not include dislocation climb, dislocation reactions or annihilations, though these will be introduced imminently. It should be noted we are not using the model to simulate plastic deformation but to investigate the lattice misorientations present in dislocation cell structures.

Figure 1. A relaxed dislocation structure with 5000 dislocations.
A dislocation model is employed to develop a kinetic law for the simulation of 3D microstructures and simulate a large distribution of dislocation densities. The model parameters such as nucleation rates and nuclei are considered.

The initial configuration consisted of a triangular lattice with periodic boundary conditions. The initial configuration was defined in terms of the sum of the dislocation energies of the system. The energy, $E$, associated with a proposed move is accepted if $\Delta E < 0$. At present we are not using the model to simulate dislocation reactions or annihilations, though we are not using the model to simulate misorientations present in dislocation cells.

Figure 1 shows the relaxed dislocation structure for a system with 5000 dislocations. There is little appearance of cell formation, though a large number of dislocation dipoles are formed. Figure 2. The skew-symmetric orientation map of the relaxed dislocation structure of figure 1.

A quantitative measure of the orientation of the lattice is given by the skew-symmetric rotation matrix:

$$\theta_{s,y} = \frac{1}{2} \left( \frac{\partial u_x}{\partial x} - \frac{\partial u_y}{\partial y} \right)$$

where $u_x$ and $u_y$ are the displacement components of each site $(x,y)$. These orientations are plotted in figure 2. A degree of cell formation is evident, although it should be noted that the relaxed structure and random configuration (not shown) share the same general features. The rotation angle, $\Delta \theta$, of each cell is defined as, $\theta_x - \theta_{ave}$, where $\theta_{ave}$ is the average orientation (very close to zero degrees in this simulation). The probability function of $\Delta \theta$ is shown in figure 3, showing that the relaxed dislocation structures have a Gaussian distribution of misorientations. We feed this result into the Cell Growth Model to generate initial microstructures.

Figure 3. The distribution of rotation angles in the dislocation model.
CELL GROWTH MODEL

We use a modified Potts model to simulate cell growth of dislocation substructures. A simulation volume is discretized into a simple cubic lattice of $N_x \times N_y \times N_z$ sites. An equiaxed cell structure is used as a starting configuration, see figure 4. Each site has a spin number $i$, where $i = 1, \ldots, N_c$ cells in the system. A set of rotation angles $m_i$ is defined which has a Gaussian distribution, and a set of axes $[uvw]_i$ are defined which are randomly distributed with a uniform probability on a unit sphere. The transformation matrix $R_i$ of a rotation of $m_i$ about $[uvw]_i$ is calculated and the orientation of each cell, $O_i$ is then given by:

$$O_i = R_i O_{ref}$$  \hspace{1cm} (3)

This procedure reproduces the distribution of orientations exhibited by the dislocation model, i.e. a Gaussian distribution with a mean of zero. Misorientations across cell boundaries are used to measure the BMD of the system which is shown in figure 5. The standard deviation of the Gaussian rotation angles, $m_i$, was found to determine the average cell boundary misorientation but did not influence the shape of the BMD which scales with average misorientation angle. At present no dynamical simulations have been carried out. Boundary migration will be implemented using a Monte Carlo Metropolis algorithm incorporating the kinetic law derived from the dislocation model.

Figure 4. The equiaxed cell microstructure

COMPARISON WITH EXPERIMENT

Dislocations developed during monotonic plastic deformation of medium to high stacking fault energy fcc metals organize into boundaries that subdivide an original grain at two length scales [9]. The larger scale is defined by long, continuous dislocation boundaries called geometrically necessary boundaries (GNBs). Within the volumes defined by these boundaries lower angle incidental dislocation boundaries (IDBs) are formed. The BMDs of GNBs and IDBs each evolve differently as a function of strain.
of dislocation substructures. A simulation of \( N \times N \) sites. An equiaxed cell structure is characterized by a spin number \( i \), where \( i = 1, \ldots, N \), which has a Gaussian distribution, and a cell orientation across a uniform probability on a unit of \([uvw]\), is calculated and the number of dislocations. A simulation of \( N \times N \) sites. An equiaxed cell structure is characterized by a spin number \( i \), where \( i = 1, \ldots, N \), which has a Gaussian distribution, and a cell orientation across a uniform probability on a unit of \([uvw]\), is calculated and the

\[
\pi_i = \frac{\sigma^2}{\theta_{av}} f\left(\frac{\theta}{\theta_{av}}\right)
\]

where \( \Gamma(\alpha) \) is the gamma function evaluated at argument \( \alpha \) (the fitting parameter), with \( \alpha = 3 \). Figure 5 shows the comparison between this curve and that constructed as a starting microstructure in the Cell Growth Model. The good correlation between the two is encouraging, however it should be noted that GNBs have not been included in the model and are likely to have an important influence on the development of recrystallization nuclei. This is the focus of our current efforts.

Figure 5. A Comparison of the BMD of the Cell Growth model with the experimentally fitted BMD
CONCLUSIONS

We have modeled the formation of dislocation sub structures by linking a dislocation model to a cell growth model. It should be noted we are not using the dislocation model to model plastic deformation, but to investigate the lattice misorientations present in dislocation cell structures. The Gaussian spread of rotation angles which comes out of the dislocation model when applied the cell model produces a BMD that is very close to the experimental BMD of IDB boundaries. The next stage will be to incorporate dynamics into the dislocation model to measure a kinetic equation for dislocation boundaries. This will then be implemented into the Cell Growth model so that the behavior of large systems cells may be studied.

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